Analyzing & Testing



Kinetic Methods for TD24 in Thermal Risk Assessment of Chemical Processes

Webinar Elena Moukhina 02/07/2023





1. Introduction. What is necessary to know and why?

2. Definitions

2.1. Characteristic temperatures of the process: Tp, MTSR, TMR, MTT2.2 Thermal Risk: primary and secondary reactions2.3 What is TD24? Why it is important?

- 3. Kinetic Methods of calculation TD24 offered by NETZSCH
 - 5.1. Theory and Examples
 - 5.2. Experimental data
 - 5.3. Kinetic Analysis
 - 5.3.1. Linear TMR Extrapolation
 - 5.3.2. Non-Linear TMR Extrapolation
 - 5.3.2. Advances kinetics by Kinetics Neo Software
- 4. Conclusion



1. Introduction. What is necessary to know and why?

Chemical industry with the thermal risk





- New materials,
- colors,
- Textiles
- Pharmaceuticals
- Nitration reactions
- Fine chemicals
- Manufacture
- Transportation
- Storage

Consecuences of thermal runaway

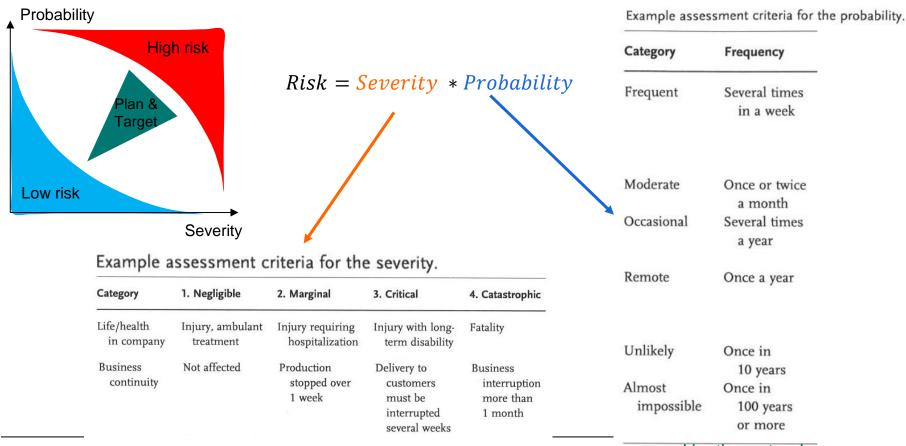




- Fire
- Explosion
- Economic loss
- Injuries and deathes

The core of risk assessment: Severity and probability





Francis Stoessel, Thermal Safety of Chemical Processes: Risk Assessment and Process Design. (Switzerland) (2008)

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- Physical properties :boiling, melting, ...
- Chemical properties: stability, ignition, sensitivity to light, air, water
- Toxicity: toxic and cancirogenic materials
- Ecotoxicity
- Fire and Explosion data: combustion, self-sustaining decomposition
- Chemical interactions: undesired reactions

Risk factors in Thermal process

- Thermal effects
 - Heat of reaction ———
 - Heat capacity -٠
 - Melting and evaporation enthalpy •
 - Adiabatic temperature rise •
 - Dependence of reaction rate on temperature -•
 - Heat removal: cooling •
- **Pressure effects**
 - Gas release
 - Vapor pressure

- **Thermal Analysis** •
 - DSC,ARC
- DSC

->>>

- DSC
 - DSC, ARC ->>>
 - Kinetic analysis: TMR approximation, **Kinetics Neo**



Risk assessment in runaway reactions





Assesment crirteria for severity of	a runaway	reaction
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Simplified Extended		ΔT_{ad} (K)	Order of magnitude of Q' kJ kg-	
High	Catastrophic	>400	>800	
	Critical	200-400	400-800	
Medium	Medium	50-100	100-400	
Low	Negligible	<50 and no pressure	<100	

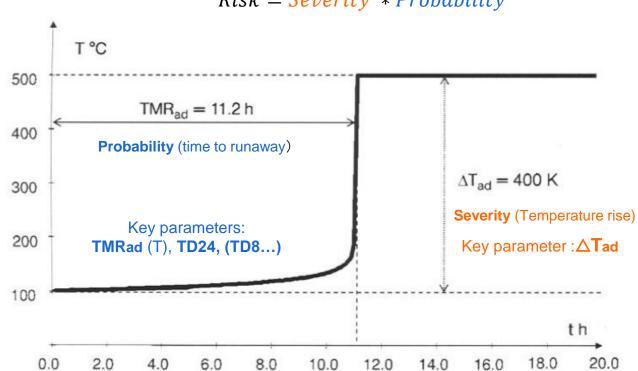
TMR_{ad} (h) Simplified Extended High Frequent <1 Probable 1-8 Medium Occasional 8-24 Seldom 24-50 Low 50-100 Remote Almost impossible >100

Assesment crirteria for probability of a runaway reaction

Francis Stoessel, Thermal Safety of Chemical Processes: Risk Assessment and Process Design. (Switzerland) (2008)

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Risk = *Severity* * *Probability*

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- a) Characteristic temperatures of the process: Tp, MTSR, TMR, MTT
- b) Primary and secondary reactions
- c) What is TD24? Why it is important?

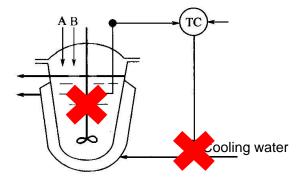


Normal process :

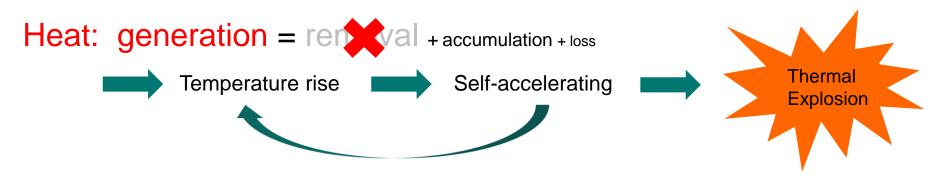
Heat: generation = removal + accumulation + loss



Temperature of reaction is under control

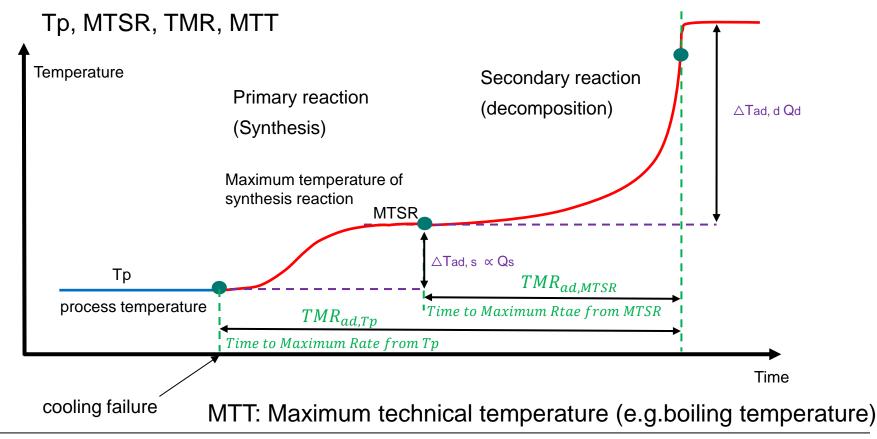


Thermal runaway :

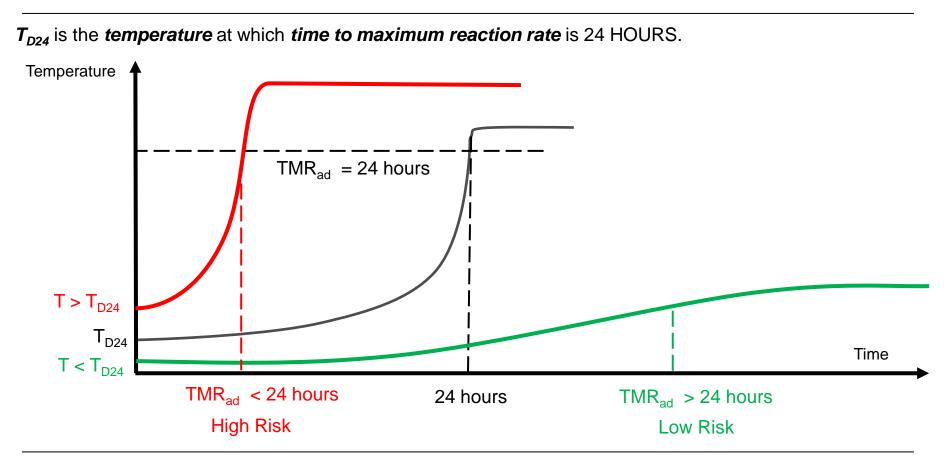


Thermal Risk for cooling failure scenario: primary and secondary reactions





Time To Maximum Rate (TMR) and T_{D24}

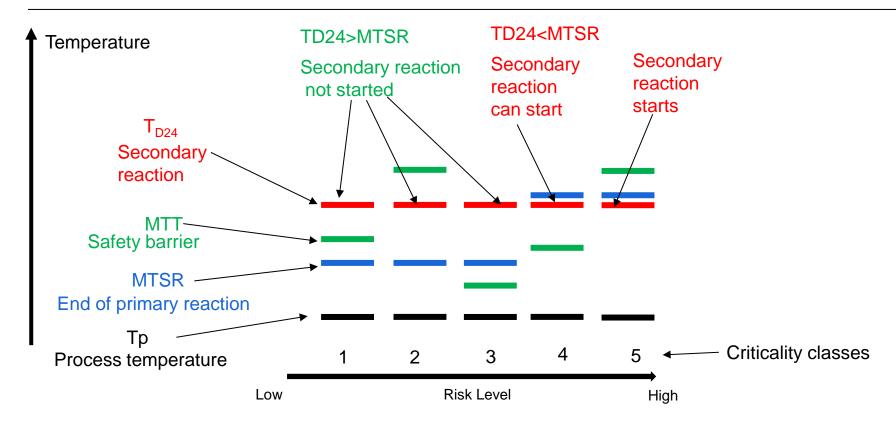


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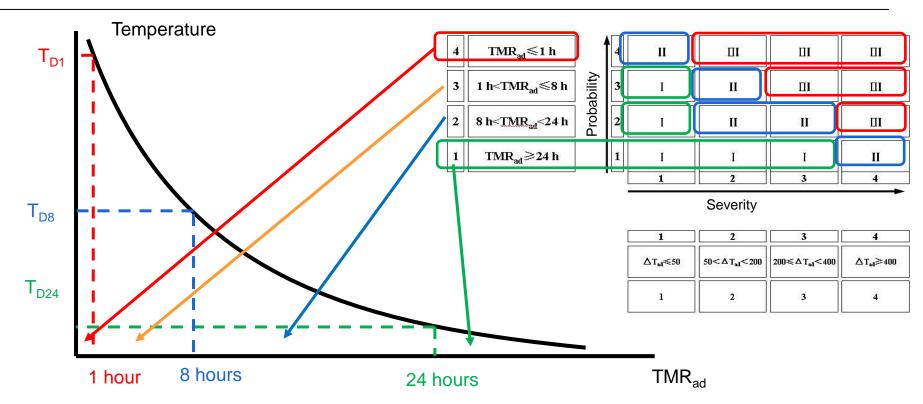
Some common methods for thermal risk assessment





Please also refer to: Thermal Safety of Chemical Processes: Risk Assessment and Process Design. by Francis Stoessel (Switzerland) (2008 inetics.netzsch com





TD24 is calculated mostly for secondary/decomposition reaction, but sometimes also for synthesis reaction, depending on the sample type (raw material, or synthesis product) and reaction process.

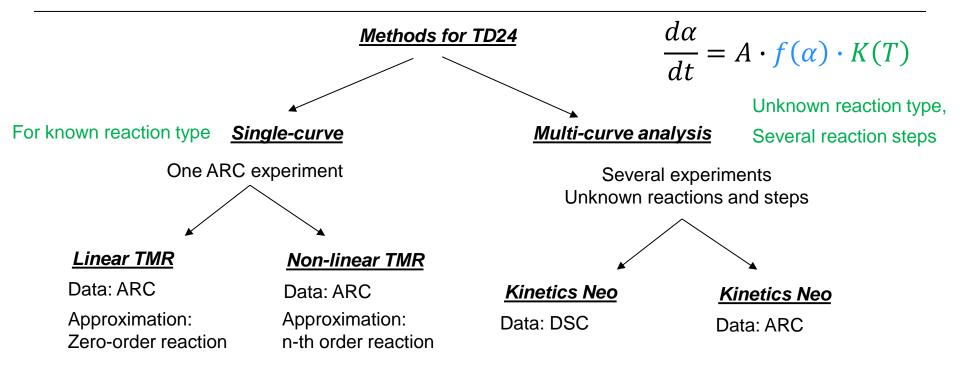


3. Kinetic Methods of calculation TD24 offered by NETZSCH

- a) Linear TMR Extrapolation
- b) Non-Linear TMR Extrapolation
- c) Advances kinetics by Kinetics Neo Software

Methods for determination of TD24 by NETZSCH instruments



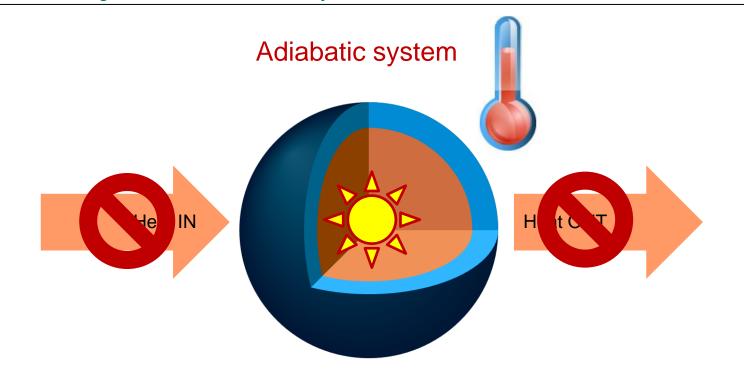






Measurements for kinetic analysis: Accelerating Reaction Calorimetry

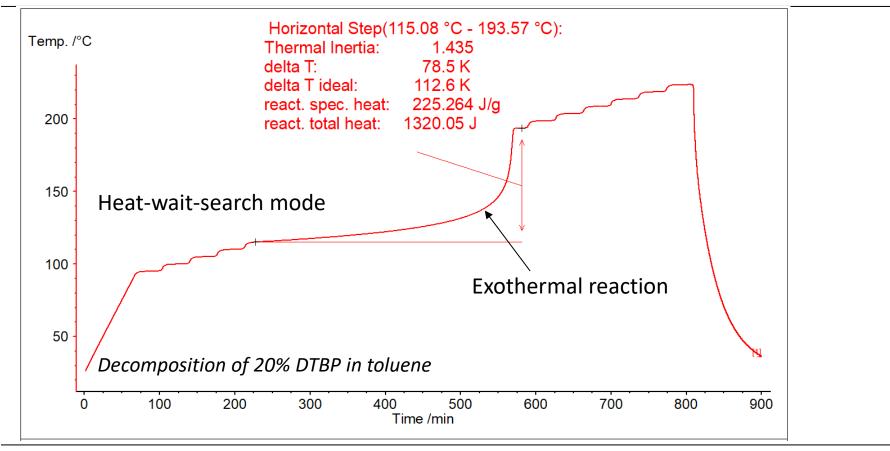




Temperature increase because of exothermal reaction

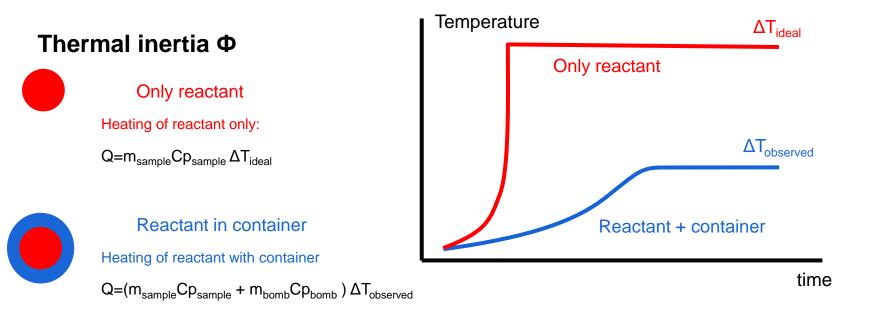
ARC data for decomposition of DTBP





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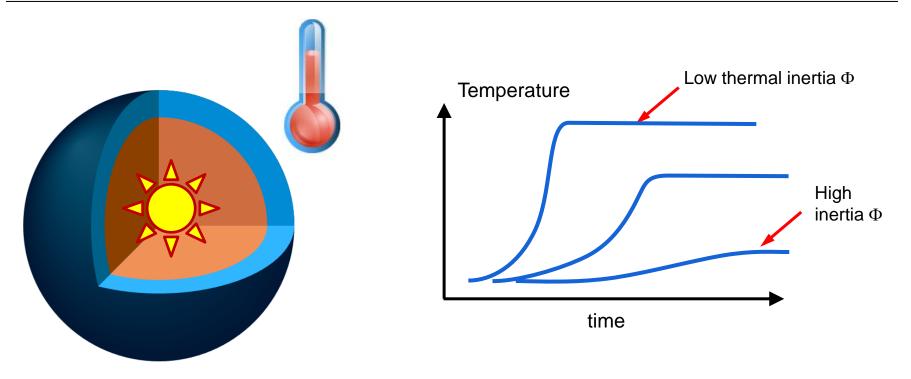


Formula for thermal inertia (Φ-factor) according to ASTM E1981:

$$\Phi = \frac{(m_{s} \cdot C_{p,s} + m_{c} \cdot C_{p,c})}{m_{s} \cdot C_{p,s}} \qquad \Phi = 1 + \frac{m_{c} \cdot C_{p,c}}{m_{s} \cdot C_{p,s}} \qquad \qquad \begin{array}{l} m_{c} = \text{mass of the container} \\ C_{p,c} = \text{heat capacity of the container} \\ m_{s} = \text{mass of the sample} \\ C_{os} = \text{heat capacity of the sample} \end{array}$$

Measurements for kinetic analysis: Accelerating Reaction Calorimetry

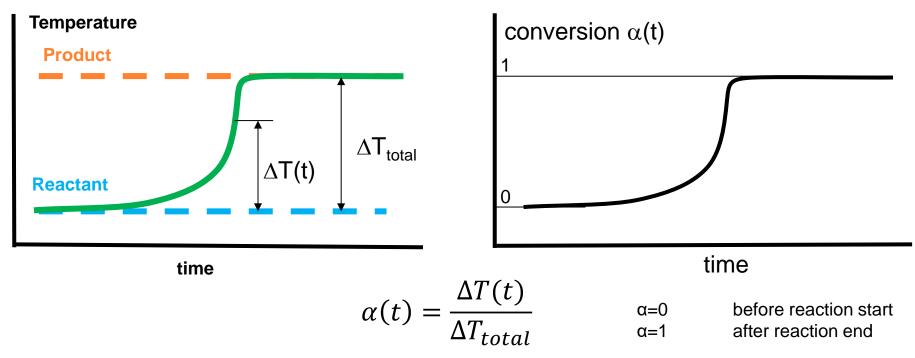




Accelerating Reaction Calorimetry: temperature change is measured during self-heating

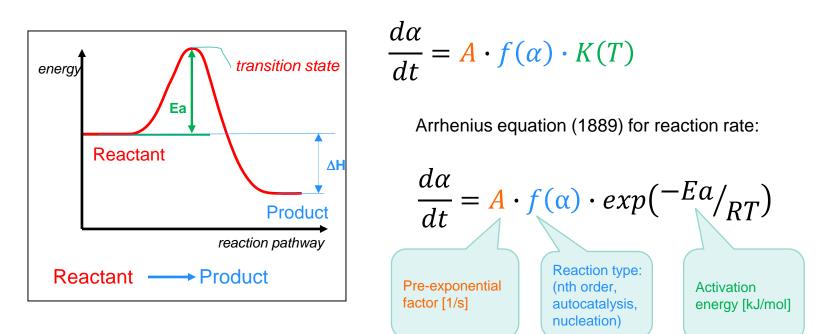
Degree of conversion α(t) for ARC data (extent of conversion, conversion, extent of reaction)

Commonly denoted by α and defined as the ratio of the partial to total change of a physical property.



ARC: Conversion is the ratio of the partial temperature increase at given time point to the total temperature increase at the final time point

Arrhenius Equation. Activation Energy. Kinetic Triplet



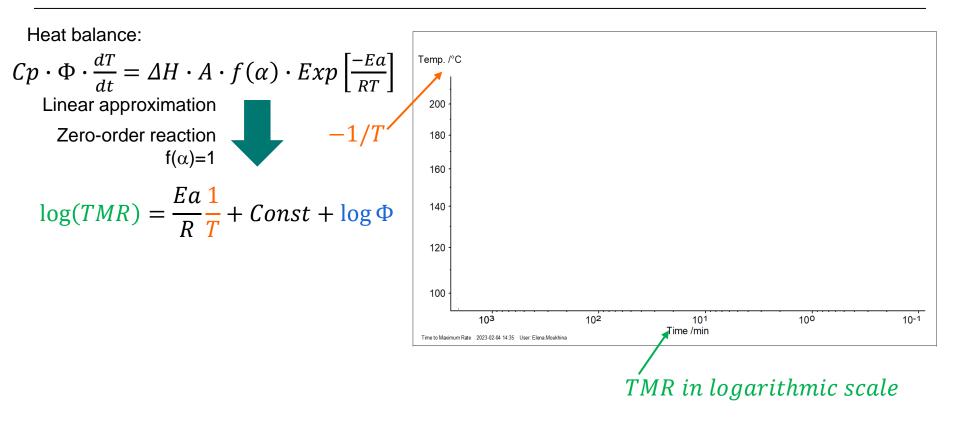
As temperature rises, the reaction rate increases exponentially!

T: absolute temperature [K]

T[K]=T[°C]+273.15

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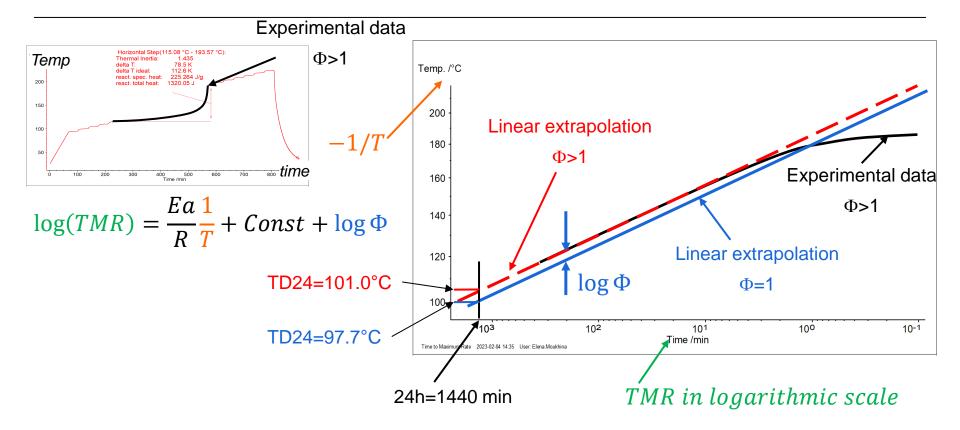
Linear TMR extrapolation for decomposition



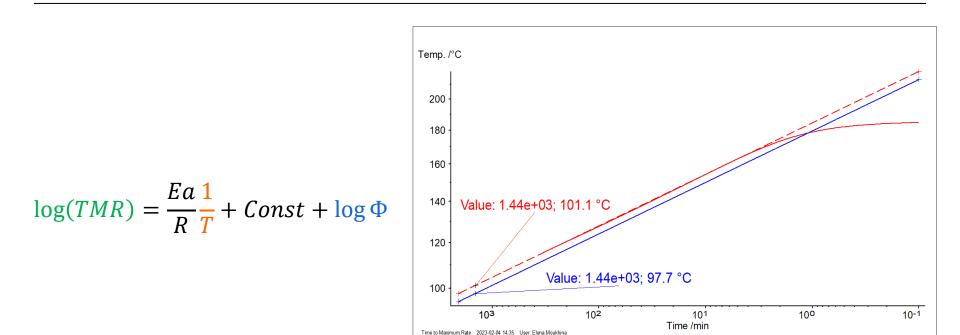


Linear TMR extrapolation for decomposition





Linear TMR extrapolation for decomposition



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NETZSCH Unique feature: Non-Linear TMR extrapolation for decomposition



Measured curve for Φ_1 has temperature step ΔT_1 and the following equation

$$\left(\frac{dT_1}{dt}\right)_{\Phi_1} = \Delta T_1 \cdot A(\alpha_1) \cdot f(\alpha_1) \cdot exp\left(\frac{-E(\alpha_1)}{RT_1}\right)$$

We would like to recalculate to the new Φ_2 with temperature step ΔT_2 :

$$\left(\frac{dT_2}{dt}\right)_{\Phi_2} = \Delta T_2 \cdot A(\alpha_2) \cdot f(\alpha_2) \cdot exp\left(\frac{-E(\alpha_2)}{RT_2}\right)$$

Recalculation of the measured temperature curve at Φ_1 to Φ_2 at the same conversion value:

$$\left(\frac{\mathrm{d}\mathrm{T}_2}{\mathrm{d}\mathrm{t}}\right)_{\Phi_2} = \left(\frac{\mathrm{d}\mathrm{T}_1}{\mathrm{d}\mathrm{t}}\right)_{\Phi_1} \cdot \frac{\Phi_1}{\Phi_2} \cdot \exp\left(\frac{-\mathrm{E}(\alpha)}{\mathrm{R}}\left(\frac{1}{T_2} - \frac{1}{T_1}\right)\right)$$

Isoconversional method is used, where the points of the same conversion are taken into account.

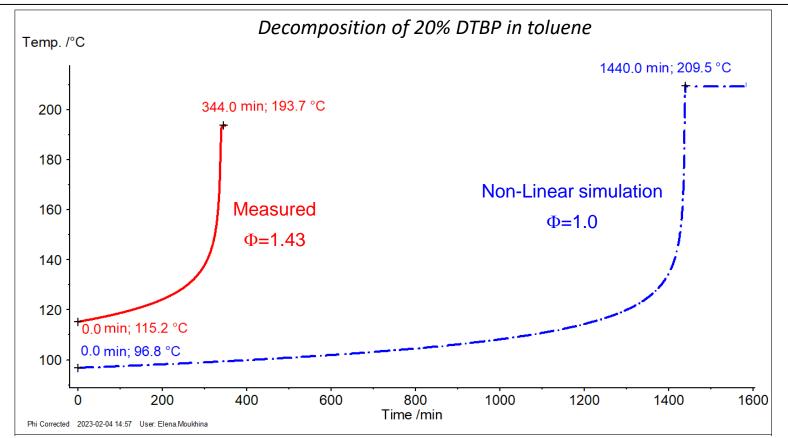
Main assumption: activation energy is the same for whole process.

Reaction type and pre-exponent are not important for this isoconversional method.

This method ensures the accuracy for whole range and makes prediction possible.

Unique feature: Non-Linear TMR extrapolation for decomposition





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Linear TMR approximation:

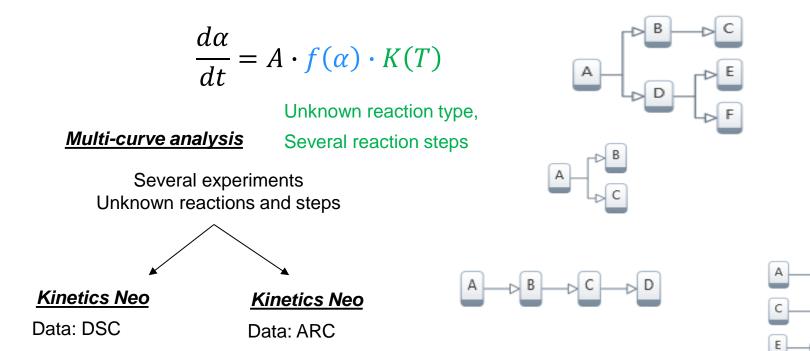
- It's based on zero-order simplification which is only valid for low-conversion regions, so the line on high-conversion region makes no sense.
- Some minor items are discarded during mathematical deduction, so the result is not so accurate.

Non-linear TMR approximation:

- The assumption for activation energy: Ea is constant for the whole process.
- The assumption of process begin as the n-th order reaction is used only for obtaining Ea from the first few points.
- No simplification for reaction type, result is more accurate.

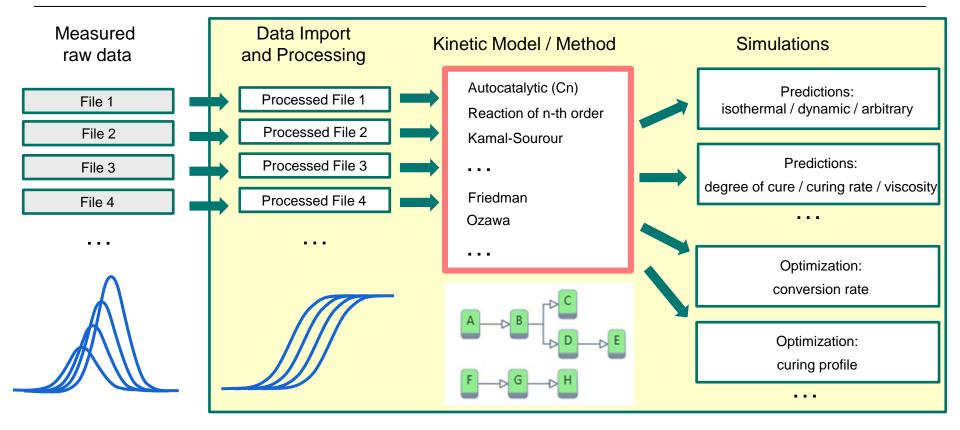
Accurate determination of TD24 by Kinetics Neo Software





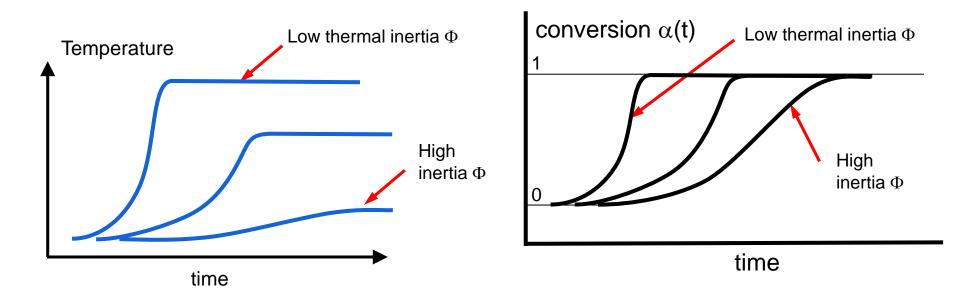
Steps to solve Kinetic Tasks in Kinetics Neo





Degree of conversion for kinetic analysis: Accelerating Reaction Calorimetry





How to change Φ ?

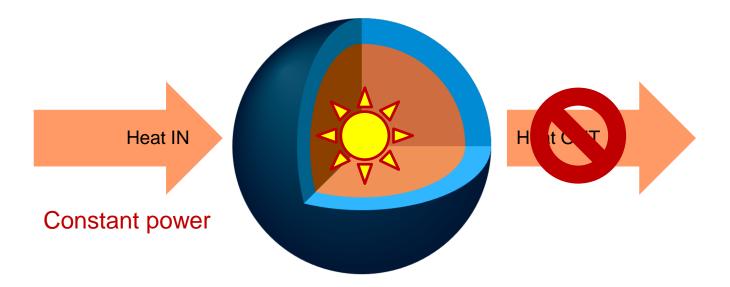
For unknown reaction the ratio between reactant mass and container mass should be different

Only for first-order reaction type the solution with solvent can be measured. Solvent increases thermal inertia

Measurements for kinetic analysis: Accelerating Reaction Calorimetry



Adiabatic system with constant power input

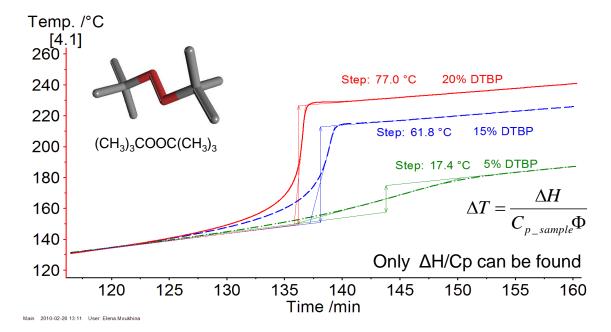


Temperature increase because of exothermal reaction and constant power input

Kinetic analysis of temperature step



Reaction causes the step on temperature curve

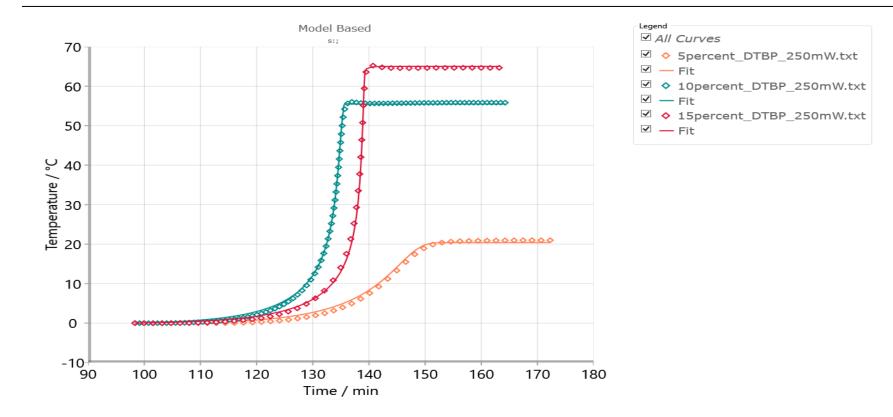


Temperature rise with different concentrations of di-tert-butil peroxid (DTBP) in toluene

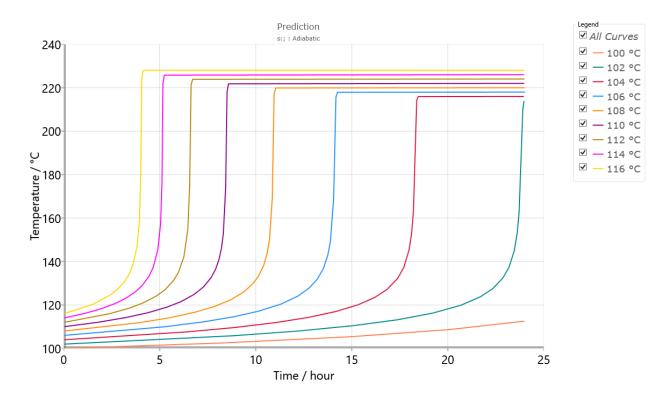
Acceleration rate calorimeter ARC 254 in VaryPhi mode with the constant underlying power 250mW.

One kinetic model for all three experiments





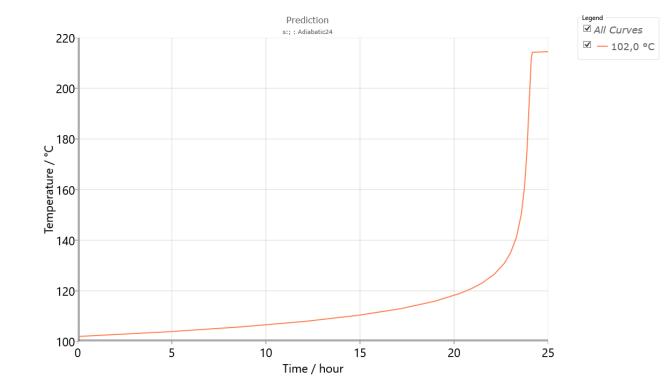
Simulation of adiabatic self-heating at different temperatures for Φ =1.0



NETZSCH

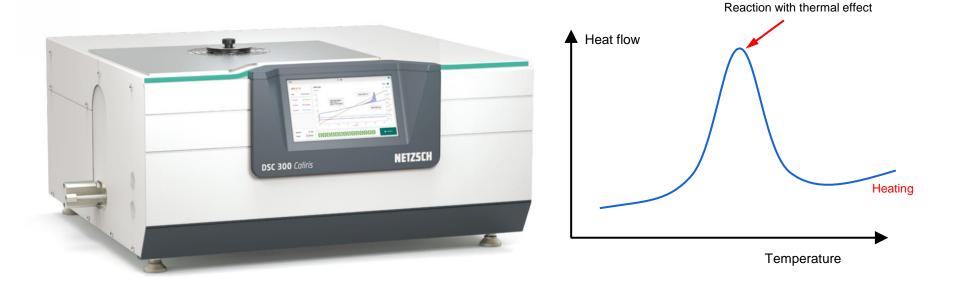
Calculation of T_{D24} for Φ =1.0 and simulation of adiabatic self-heating at this temperature





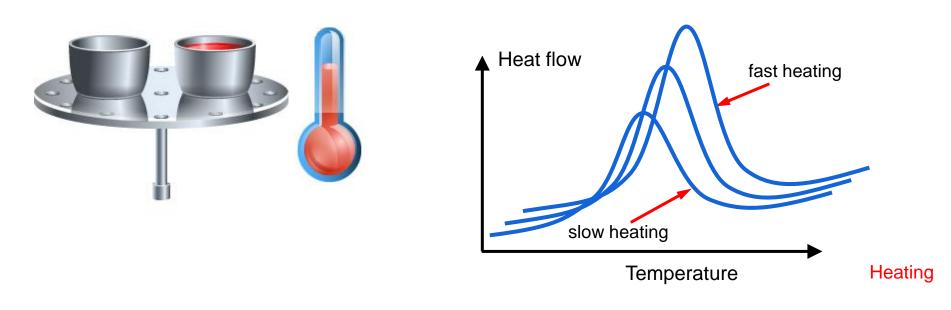
DSC: Differential Scanning Calorimetry





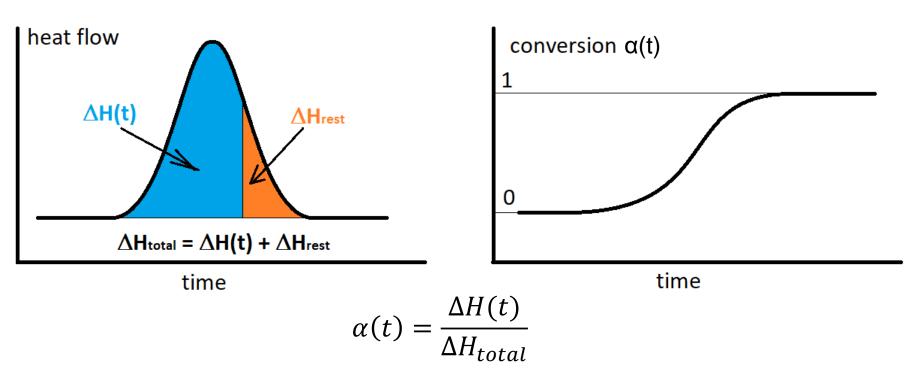
Measurements for kinetic analysis: Differential scanning calorimetry





Differential scanning calorimetry: heat flow is measured during temperature





DSC: Conversion is the ratio of the partial enthalpy change at given time point to the total enthalpy change at the final time point



Arrhenius equation

$$\frac{d\alpha}{dt} = \mathbf{A} \cdot f(\alpha) \cdot exp\left(\frac{-E_A}{RT}\right)$$

Reaction of n-th order is typical for decomposition

Fn
$$\frac{d\alpha}{dt} = A \cdot \underbrace{(1-\alpha)^n} \exp\left(\frac{-E_a}{RT}\right)$$

Reaction types: reactions with autocatalysis

Chemical process is **generally** described by Arrhenius equation:

$$\frac{d\alpha}{dt} = \mathbf{A} \cdot f(\alpha) \cdot exp\left(\frac{-E_A}{RT}\right)$$

<u>Bna</u> – autocatalytical reacton of Prout-Tompkins

$$\frac{d\alpha}{dt} = A \cdot (1 - \alpha)^n \cdot \exp\left(\frac{-E_a}{RT}\right) \cdot \alpha^m$$

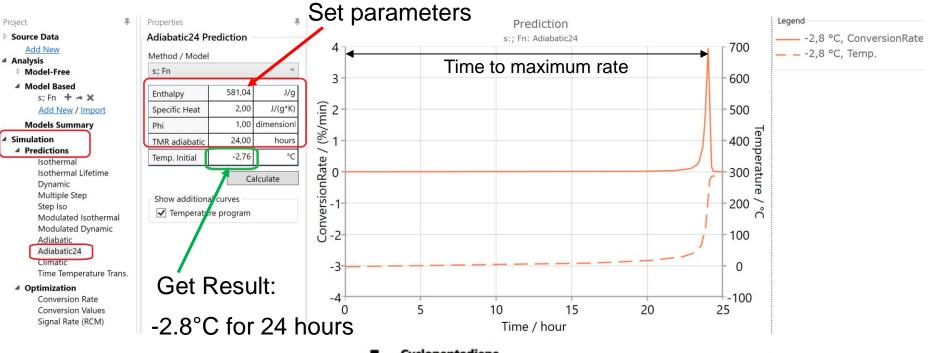


Curing can be described by the equation Kamal-Sourour for autocatalytic reaction: $\frac{d\alpha}{dt} = A \cdot (1 - \alpha)^n \cdot \exp\left(\frac{-E_{a1}}{RT}\right) + A \cdot K \cdot (1 - \alpha)^n \cdot \alpha^m \cdot \exp\left(\frac{-E_{a2}}{RT}\right)$ n-th order
autocatalysis
autocatalysis

This equation with its parameters A, E_{a1} , n, E_{a2} , K, m, is the kinetic model.



Cyclopentadiene: What is the initial temperature for TMR=24 hours for Phi=1.0?



"The conversion occurs in hours at room temperature, but the monomer can be stored for days at -20 °C"

Hönicke, Dieter; Födisch, Ringo; Claus, Peter; Olson, Michael. "Cyclopentadiene and Cyclopentene". <u>Ullmann's Encyclopedia of Industrial Chemistry</u>. Weinheim: Wiley-VCH.

Cyclopentadiene

 Can polymerise, but its main danger lies in its propensity to dimerise by the Diels-Alder reaction. This reaction takes place at a temperature starting at 0-40°C, under pressure. If the dimerisation is not controlled, the storage equipments' temperature and pressure rise very quickly, which leads to their destruction. Storage temperatures of -80°C have been recommended.

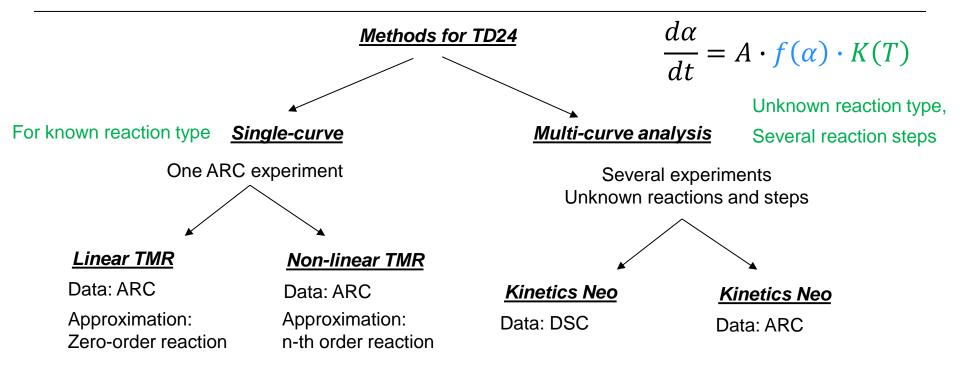
Book: Bernand Martel, Chemical Risk Analysis, 1988

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Methods for determination of TD24 by NETZSCH instruments





You can rely on NETZSCH.

NETZSCH Proven Excellence.

elena.moukhina@netzsch.com

www.kinetics.netzsch.com kinetics.neo@netzsch.com